



INFLUENCE OF NANOPARTICLE CaCO_3 ADDITION TO THE PHYSICAL AND MECHANICAL PROPERTIES OF POLYPROPYLENE- CaCO_3 COMPOSITE

Deswita*¹, Yusmaniar², Grace Tj. Sulungbudi¹, Aloma Karo Karo¹. and Sudirman¹

¹National Innovation and Research Agency, BRIN
Kawasan Puspiptek, Serpong, Tangerang, Banten 15314

²Universitas Negeri Jakarta
Jl. Pemuda No.10 Jakarta

*Corresponding author
Email: deswita@batan.go.id

Abstract. *Influence of Nanoparticle CaCO_3 Addition to the Physical and Mechanical Properties of Polypropylene- CaCO_3 Composite. This research was carried out to study the effect of adding CaCO_3 nanoparticle on the physical and mechanical properties of polypropylene- CaCO_3 composites. It was characterized by several parameters such as tensile strength, hardness, and thermal analysis including both melting point and heat of fusion using Differential Scanning Calorimetry (DSC). Based on XRD results, the particle size of CaCO_3 after 24 hours of milling was 39 nm. There are various compositions of polypropylene- CaCO_3 composites (PP MF35: nano- CaCO_3) made in this study, namely 40%:60%, 35%:65%, 30%:70%, and 25%:75%. The results showed that the tensile strength of the PP MF35- CaCO_3 composites decreased with increasing nano- CaCO_3 content. Meanwhile, the hardness of the nanocomposites increased with increasing nano- CaCO_3 content, but decreased the melting point and heat of fusions (ΔH_m) of the nanocomposites. The infrared spectrum showed that the interaction between PP MF35 and nano- CaCO_3 was only physical interaction and there was no chemical reaction.*

Keywords: *polypropylene; nano- CaCO_3 ; tensile strength; composite.*

1. Introduction

An increasing population is always followed by an increase in the necessities of life. This is what underlies the increasing need for plastic as a packaging of food, beverage and other necessities. By 2050, it is estimated that the world's population will reach 9 billion and the level of plastic production will exceed 1 billion tons.

Plastic as a packaging has several advantages such as strong, light, transparent, stainless, easy to shape and to color and also has a low price. Plastics can be applied in various human life sector like household, automotive, agriculture and health [1]. Market demand for good quality goods at competitive prices and the increasingly rapid development of polymer technology have prompted scientists to make polymer-based plastics by mixing polymers with nano-sized fillers. In this research, a polymer composite was made by mixing polypropylene as a matrix and CaCO_3 as a filler.

Polypropylene (PP) is a type of thermoplastic polymer, which is a linear hydrocarbon polymer formed by propylene monomers. In this study, polypropylene was used because it is widely used as a raw material of packaging for food, beverages and other applications [2]. One of the fillers that can be applied is CaCO_3 . It is used because the presence of CaCO_3 in nature is abundant, cheap, inert and it has high melting point. The economic price of the filler causes the final product price to be lower, so that economically, it will benefit producers and consumers [3]. CaCO_3 as a filler is made in nanometer size. Because the smaller the size of filler particle, it is expected that the more filler can interact with the matrix, so that the less polymer matrix is applied. Moreover, it caused changes in the physical and mechanical properties of polypropylene. It can improve the physical and mechanical properties of polypropylene [3]. Based on previous research, the addition of micro-sized CaCO_3 reduces the mechanical properties of PP- CaCO_3 composites. Meanwhile, both tensile strength and flexural strength of Polyethylene-terephthalate (PET)/Polypropylene (PP)/ CaCO_3 are increased after the addition of specific composition of CaCO_3 . [5]. It also improved the melting point of polypropylene [6]. Therefore, the effect of nano-sized CaCO_3 on properties of PP MF35- CaCO_3 nanocomposites was investigated in this study [4–6].

2. Experimental Methods

2.1. Materials

The polypropylene with melt flow of 35g/10 min is a product of PT TRI POLYTA INDONESIA, Tbk, Cilegon – Banten. Calcium carbonate (pro analyzed) used the (MERCK catalog) as a filler, Yasicha brand mica plastic and nitrogen liquid.

2.2. Experimental Procedure

2.2.1. Manufacture of Nano-sized CaCO_3

High Energy Mill (HEM, brand SPEX Centriprep 8000-series Mixer/Mills) is used to manufacture nano-sized CaCO_3 . First of all, CaCO_3 and sphere go tri with weight ratio of 1:2 was put into vial and then milled with HEM to obtain a nanometer size. After that, the milling process was carried out with different time variations such as 0, 6, 12, 18 and 24 hours on different samples.

2.2.2. Synthesis of PP MF35- CaCO_3 Composite

First of all, laboplastomill (Toyoseiki brand, Japan) is cleaned with acetone to avoid impurities during material synthesis. Then, mix the melted polypropylene 35 with nano-sized CaCO_3 in laboplastomill at a temperature of 1800°C for 10 minutes with a rotating speed of 40 rpm. The variations of CaCO_3 are 60, 65, 70, and 75wt% and the propylene of 25, 30, 35, and 40wt%. After mixing homogeneously, then the mixture was made a film using Hydraulic Hot Press at a temperature of 1800°C for 5 minutes and a pressure of $150\text{kg}/\text{cm}^2$. Then the film molding tool is put into the cold pressing machine (a/s 16 Tons Hydraulic Press).

2.2.3. Characterization.

The manufacture of nano-sized CaCO_3 is carried out using High Energy Mill (HEM) for 24 hours to minimize the particle size of material. The particle size of CaCO_3 after milling for 24 hours were measured using X-Ray Diffraction (XRD-PAN Analytical 610) with $\text{Cu-K}\alpha$ source at wavelength (λ) = 0.154 nm). Infra-red (IR) spectrum for identification of functional groups and metal oxide bonds was measured by means of Fourier Transformation Infra-Red (FTIR) type Tensor 27 Bruker. Samples in powder form as much as 5 mg were mixed with KBr then crushed and homogenized and then pressed to form pellets. Samples were irradiated with IR in the wave number range of 500 cm^{-1} to 3000 cm^{-1} .



Figure 1. Specimen of the tensile test.

Tensile strength specimens were produced by using the TKC series-vertical injection mold machine, following the ASTM D638 standard. The tensile specimen size was 19 mm wide, 113 mm length, and thickness 4 mm (Fig. 1). Five samples were tested for each composition. The experiment was carried out on Strogaph R1, Toyoseiki (Japan) with longitudinal extension, a high resolution ($1.8\ \mu\text{m}$). Some basic specifications are described as follows: The maximum test power was 20 kN, in range of speed 0.001-1600 mm/min, speed accuracy $\pm 0.1\%$ test speed, the operating temperature at $5\text{-}50^\circ\text{C}$, data acquisition speed 1000 Hz. SEM characterization was carried out to determine the morphology, microstructure and particle size distribution of the CaCO_3 , the test was carried out with a magnification of 5000 times using a SEM- JEOL 6510 LA.

3. Result and Discussion

3.1. Manufacture of Nano-sized CaCO_3

The manufacture of nano-sized CaCO_3 is carried out using High Energy Mill (HEM). In HEM, there is a process of CaCO_3 attrition. The attrition method is a method in which micrometer-sized material is hammered into a particular ball milling in order to minimize the particle size of material [7]. So that finally we get a material with a smaller particle size (in nanometers).

The results of the measurement of the x-ray diffraction pattern from the mechanical milling process which are expected to form CaCO_3 nanoparticles are shown in Figure 2. Figure 2 shows the x-ray diffraction pattern with milling time variations of 0, 6, 12, 18, and 24 hours. Phase

identification shows that the sample after milling has an unchanged phase, in other words, that milling does not find any foreign phase. In this research, particle size analysis used X-ray diffraction using the Scherer method in which the crystalline scale is determined based on the reaming of the X-ray diffraction peaks that appear. Based on this method, the more small-scale crystals, the wider the diffraction peaks will be. The relationship between scale crystals and X-ray peak diffraction width can be seen with the Scherer equation [8]:

$$D \approx K \frac{\lambda}{B \cos \theta_B} \dots\dots\dots(1)$$

Where D is crystallite size in nano-meter; κ a constant whose value depends on particle shape; B is FWHM (Full Width at Half Maximum); λ is the wavelength of incident beams in nm and θ is Bragg’s angle. Based on result of gauging at milling 24 hours, we obtained that the average D value of CaCO₃ after milling for 24 hours was about 39 nm.

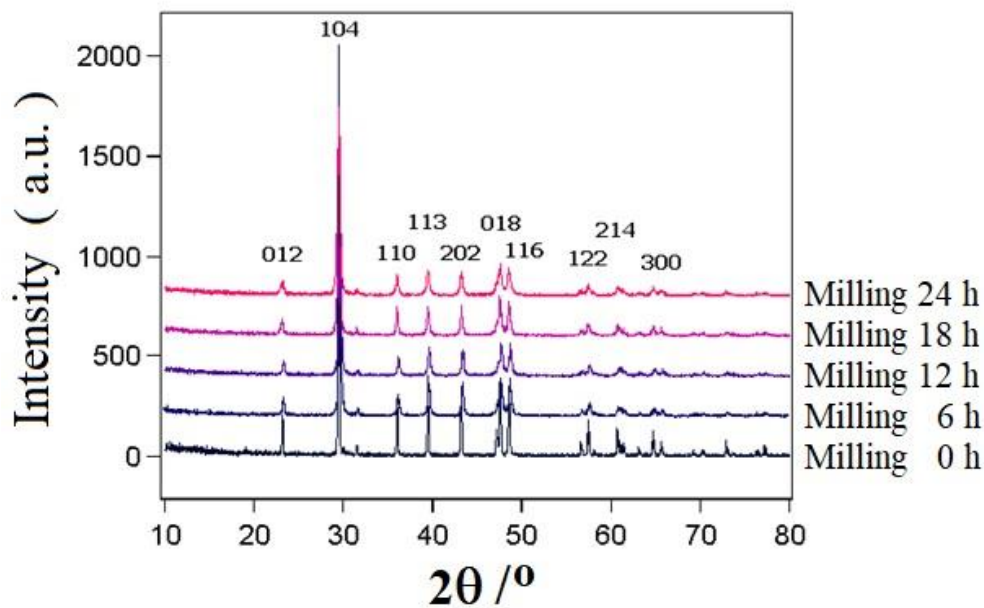


Figure 2. X-ray diffraction pattern of CaCO₃ milling time variation.

3.2. Analysis of Mechanical Properties (Tensile Strength)

The tensile was the tensile properties that were determined using five samples for each composition to study the effect of CaCO₃ on tensile properties. Tensile strength specimens were produced by using the TKC series-vertical injection mold machine, following the ASTM D638 standard. Tensile strength can be determined by applying force to the test material until it breaks. Tensile strength, which is a measure of the ability of a polymer to withstand pulling stresses is usually measured by pulling a dumbbell specimen [9,10].

Table 1. Tensile Strength of PPMF35+CaCO₃

No.	Samples	Heat of Fusions (J/g)
1.	PP MF35	283
2.	PPMF35-40% + 60% CaCO ₃	181
3.	PP MF35-35% + 65% CaCO ₃	148
4.	PP MF35-30% + 70% CaCO ₃	125
5.	PP MF35-25% + 75% CaCO ₃	87

Based on the results above, it is known that the tensile strength decreased with the increasing of nano-sized CaCO₃ filler content. Meanwhile, it decreased due to uneven distribution of nano-sized CaCO₃. This is because nano-sized CaCO₃ filler has very small particles, so that the nano-sized CaCO₃ tends to clump and form a larger drain structure or known as agglomeration which has an impact on the decreasing of tensile strength [9,11]. The tendency to form very large agglomerates is due to electrostatic forces between CaCO₃ particles. Particles with a diameter of less than 1 μm have a relatively high tendency for agglomeration to occur.

Polypropylene MF35/nano-CaCO₃ composite have tensile strength with higher level if compared to PP MF35-CaCO₃ composite at the same concentration. PP MF35-CaCO₃ composite at concentration of CaCO₃ equal to 60% have the tensile strength at about 148kg/cm². Meanwhile, tensile strength of PP MF35/nano-CaCO₃ composite at concentration of CaCO₃ 60% is about 181kg/cm². The increase of tensile strength is equal to 18%. This caused by filler nanometer CaCO₃ which has big equi-amplitude surface district so that it will give more contact between filler and matrix resulting mechanical properties of polymers composite to increase [12].

3.3. Analysis of Physical Properties

3.3.1. Hardness

Hardness is the resistance to local deformation that is often measured as the ease or difficulty for a material to be scratched, indented, marred, cut, drilled, or abraded. In this research, hardness was measured by Shore A.

Tabel 2. Hardness of PPMF35/CaCO₃

No.	Samples	Heat of Fusions (J/g)
1.	PP MF35	91
2.	PP MF35 40% + 60% nano-CaCO ₃	92
3.	PP MF35 35% + 65% nano-CaCO ₃	93
4.	PP MF35 30% + 70% nano-CaCO ₃	94
5.	PP MF35 25% + 75% nano-CaCO ₃	95

Based on the table, the hardness of the composites increased with the increasing of nano-CaCO₃ composition because the addition of CaCO₃ can increase the molecular weight of the polymer so that it can also increase the solidity of polymer. Consequently, it increased the crystallinity of polymer [13].

3.3.2. Analysis of Thermal

The analysis of thermal properties includes melting point (T_m) and heat fusion (ΔH_m) using Differential Scanning Calorimetry (DSC, Perkin Elmer Brand) method. Melting point describes the phase transformation from solid to liquid without undergoing a transformation of the composition. Melting is basically the separation of polymer chains in a crystalline region which allows the polymer to flow.

Table 3. Melting Point of PP MF35/Nano-CaCO₃

No.	Sample	Heat of Fusions (J/g)
1.	PP MF35 40% + 60% nano-CaCO ₃	160
2.	PP MF35 35% + 65% nano-CaCO ₃	158
3.	PP MF35 30%+ 70% nano-CaCO ₃	159
4.	PP MF35 25%+ 75% nano-CaCO ₃	156

Tabel 4. Heat of fusion of composite PP MF35/nano-CaCO₃

No.	Sample	Heat of Fusions (J/g)
1.	PP MF35 + 60% nano-CaCO ₃	25
2.	PP MF35 + 65% nano-CaCO ₃	22
3.	PP MF35 + 70% nano-CaCO ₃	20
4.	PP MF35 + 75% nano-CaCO ₃	14

Based on the Table 4, the melting point of nanocomposites decreased with the increasing of nano-CaCO₃ filler content. This is because the polymer chain was physically degraded and was released to the wall together with the filler, causing the breakdown of the polymer molecular chain bonds. The addition of filler to polymer matrix shows that the interaction of filler with the amorphous part of PP MF35 was also increasing, so that it reduced the crystallinity of PP MF35 and its melting point [14].

The reduction of heat fusion occurred due to the higher concentration of nano-CaCO₃ in the composites. As a result, the concentration of PP MF35 in the composite reduced, then it also reduced the required energy to break polymer chains of PP MF35 when it changed from a solid to liquid state.

3.3.3. Analysis of Functional Groups with Fourier Transform Infra-Red (FT-IR)

FT-IR analysis is applied to identify organ compounds based on readings of the functional groups of the compounds in the form of spectrum read on the graph. Polypropylene, CaCO₃, and PP/nano-CaCO₃ composites were identified for functional groups using FT-IR.

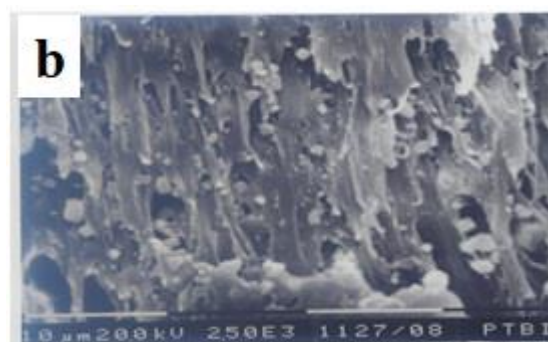
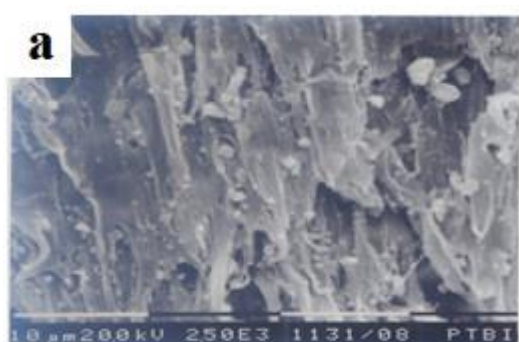
Based on spectral data, we see the absorption peak at wave number around 3382cm⁻¹ which is a stretching vibration absorption of primary NH₂, NH stretching vibration absorption at wave numbers around 1570cm⁻¹, and aliphatic CH vibration absorption at wave numbers around 2800 - 3000cm⁻¹. Si-OC vibrations identified in the wave numbers 1100 and 1085 cm⁻¹. O-CH₃ vibrations identified in the wave numbers 1450 and 1434 cm⁻¹. CH₂ bending vibrations identified in the wave numbers around 1485 and 1150-1162cm⁻¹ while the C-CH₃ bending identified in the wave numbers 1382, 1337 and 958cm⁻¹.

Table 5. Infrared spectrum of PP MF35/nano-CaCO₃ composite

No.	Group	Wavenumber (cm ⁻¹)
1.	C-H stretching	2800-3000
2.	CH ₂ bending	1162
3.	CH ₃ bending	1382, 1337 and 958

3.3.4. Distribution Nano-CaCO₃ in Polymers Composite

Figure 1 showed the morphology of CaCO₃ which was observed using Scanning Electron Microscopy (SEM). CaCO₃ undergoes agglomeration due to its small scale. Based on figure 1, the cupola of volume diffraction composition of PP MF-35/nano-CaCO₃ (40wt%/ 60wt%) looks a bit slippery, rather flat, rather dense and looks rather compact when compared to the addition of volume diffraction greater than 60wt%. With the addition of the diffraction percentage of the CaCO₃ filler composition into the nanocomposite, the real composition will be greater and larger chambers. Meanwhile, its distribution is more coarse, uneven, and not compact. This is due to the influence of nano-CaCO₃ which tends to agglomerate [15].



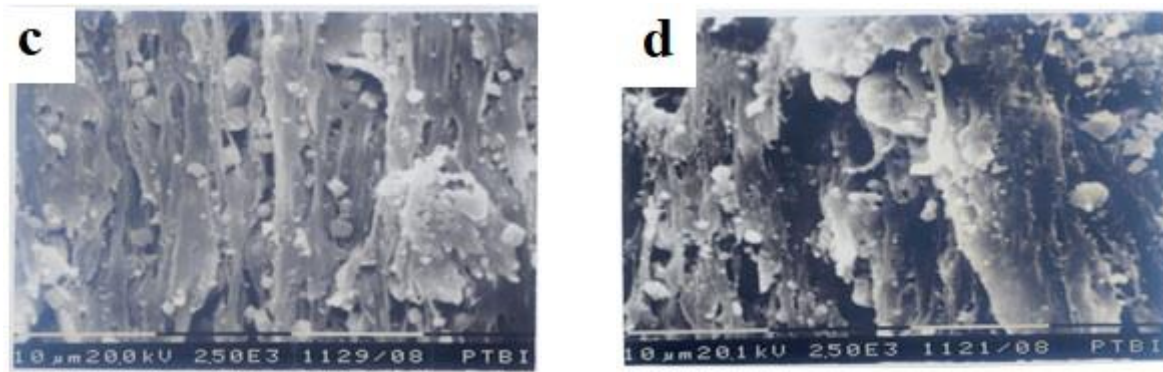


Figure 1. SEM image of nano- CaCO_3 distribution in polypropylene- CaCO_3 composite. (a) in composition PP MF35 60%-40% CaCO_3 (b) in composition PP MF35 65%-35% CaCO_3 (c) in composition PP MF35 70%-30% CaCO_3 and (d) in composition PPMF35 75%-25% CaCO_3 .

3. Conclusion

Based on XRD results, the particle size of CaCO_3 after 24 hours of milling was 39 nm. The tensile strength of the PP MF35- CaCO_3 composites decreased with the increasing of nano-sized CaCO_3 filler content. Meanwhile, the hardness of the nanocomposites increased with the increasing of nano-sized CaCO_3 filler content, but both the melting point and the heat of fusions (ΔH_m) the nanocomposites decreased. The infrared spectrum showed that the interaction between PP MF35 and nano- CaCO_3 was only physical interaction and there was no chemical reaction occurred.

4. References

- [1] A. Pratap and D. A. Sarjubala, "Microplastics and single use plastics: A curse of over consumerism," *Int. J. Adv. Sci. Res. Manag.*, vol. 4, no. 4, pp. 384–388, 2019, [Online]. Available: www.ijasrm.com.
- [2] G. W. Curtzwiler, M. Schweitzer, Y. Li, S. Jiang, and K. L. Vorst, "Mixed post-consumer recycled polyolefins as a property tuning material for virgin polypropylene," *J. Clean. Prod.*, vol. 239, p. 117978, 2019, doi: <https://doi.org/10.1016/j.jclepro.2019.117978>.
- [3] H. P. S. Abdul Khalil *et al.*, "Microbial-induced CaCO_3 filled seaweed-based film for green plasticulture application," *J. Clean. Prod.*, vol. 199, pp. 150–163, 2018, doi: <https://doi.org/10.1016/j.jclepro.2018.07.111>.
- [4] H. Mao, B. He, W. Guo, L. Hua, and Q. Yang, "Effects of Nano- CaCO_3 content on the crystallization, mechanical properties, and cell structure of PP nanocomposites in microcellular injection molding," *Polymers (Basel)*, vol. 10, no. 10, 2018, doi: <https://doi.org/10.3390/polym10101160>.
- [5] H. N. T. Pham and V. T. Nguyen, "Effect of calcium carbonate on the mechanical properties of polyethylene terephthalate/polypropylene blends with styrene-ethylene/butylene-styrene," *J. Mech. Sci. Technol.*, vol. 34, no. 10, pp. 3925–3930, 2020, doi: <https://doi.org/10.1007/s12206-020-2201-1>.
- [6] X. Jing, W. Gong, Z. Feng, M. Zhang, X. Meng, and B. Zheng, "Novel Comb-Like

- Copolymer Dispersant for Polypropylene/CaCO₃ Composites and Its Influence on Dispersion, Crystallization, Mechanical, and Thermal Properties,” *Polym. - Plast. Technol. Eng.*, vol. 57, no. 10, pp. 986–996, 2018, doi: <https://doi.org/10.1080/03602559.2017.1370105>.
- [7] A. P. Nugroho, Masruroh, and S. P. Sakti, “The design and optimization process of ball mill to reduce particle size of calcium carbonate materials,” *AIP Conf. Proc.*, vol. 2296, no. November 2020, pp. 5–10, 2020, doi: <https://doi.org/10.1063/5.0030531>.
- [8] S. J. Tracy, S. J. Turneure, and T. S. Duffy, “In situ X-Ray Diffraction of Shock-Compressed Fused Silica,” *Phys. Rev. Lett.*, vol. 120, no. 13, p. 135702, 2018, doi: <https://doi.org/10.1103/PhysRevLett.120.135702>.
- [9] S. Samal, “Effect of shape and size of filler particle on the aggregation and sedimentation behavior of the polymer composite,” *Powder Technol.*, vol. 366, pp. 43–51, 2020, doi: <https://doi.org/10.1016/j.powtec.2020.02.054>.
- [10] J. Yu and C. K. Y. Leung, “Using Limestone Calcined Clay to Improve Tensile Performance and Greenness of High-Tensile Strength Strain-Hardening Cementitious Composites (SHCC),” *Calcined Clays Sustain. Concr.*, p. 2020, 2020.
- [11] Y. Kezuka and M. Tajika, “Fracture strength evaluation of agglomerates of fatty acid-coated caco₃ nanoparticles by nano-indentation,” *ChemEngineering*, vol. 3, no. 3, pp. 1–9, 2019, doi: <https://doi.org/10.3390/chemengineering3030073>.
- [12] C. Budiyanoro, H. Sosiati, B. P. Kamiel, and M. L. S. Fikri, “The effect of CaCO₃ filler component on mechanical properties of polypropylene,” *IOP Conf. Ser. Mater. Sci. Eng.*, vol. 432, no. 1, 2018, doi: <https://doi.org/10.1088/1757-899X/432/1/012043>.
- [13] M. Barczewski *et al.*, “Thermo-mechanical and mechanical behavior of hybrid isotactic polypropylene glass fiber reinforced composites (GFRC) modified with calcium carbonate (CaCO₃),” *Polym. Eng. Sci.*, vol. 60, no. 7, pp. 1588–1603, 2020, doi: <https://doi.org/10.1002/pen.25404>.
- [14] E. A. Bilalova, E. V. Prut, and O. P. Kuznetsova, “Polypropylene composite material and its rheological and mechanical properties depending on the size of the filler CaCO₃,” *IOP Conf. Ser. Mater. Sci. Eng.*, vol. 525, no. 1, 2019, doi: <https://doi.org/10.1088/1757-899X/525/1/012006>.
- [15] O. Ersoy and H. Köse, “Comparison of the effect of reactive and nonreactive treatments on the dispersion characteristics of a calcium carbonate (calcite) filler in a polypropylene matrix composite,” *Polym. Compos.*, vol. 41, no. 9, pp. 3483–3490, 2020, doi: <https://doi.org/10.1002/pc.25634>.